

Technical Field

Background

The control techniques used to eliminate rotor position, velocity or flux sensors are often described as "sensorless control." At high rotor

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speeds and excitation frequencies, these techniques have shown a lot of promise and have achieved some commercial success. Their inability to run at lower speeds and excitation frequencies excludes these techniques from being used in applications that require operation in these regions, including industrial drives, consumer appliances, and automotive applications (for example, electric traction drives for electric or fuel cell powered vehicles, hybrid electric vehicles, and electric power assisted steering).

To overcome the inability of operating at low rotor speeds and excitation frequencies, a second class of "sensorless controls" techniques has been developed that eliminates the dependence on the fundamental excitation of the electric machine. These techniques use a separate, high frequency sensing excitation applied to the machine in addition to fundamental excitation. There are many forms that the sensing excitation can take, but a fundamental requirement for those techniques to work is that the electric machine must have some form of saliency. For rotor position or velocity estimation, the saliency must have been related to and move when the rotor of the machine moves. For flux estimation, the saliency typically has some saturation-related dependence and hence contains information related to the position of the flux in the machine. Some examples of these machine types include synchronous reluctance machines, buried permanent magnet machines, switch reluctance machines, and salient pole synchronous machines.

process, manufacturing techniques are greatly simplified, thereby decreasing the costs associated with manufacturing the rotor.

Other objects and advantages of the present invention will become apparent upon considering the following detailed description and appended claims, and upon reference to the accompanying drawings.

Brief Description of the Drawings

Figure 1 depicts a top view of a stator and rotor of an electric machine drive having a plurality of rotor sensing slots according to one preferred embodiment of the present invention;

Figure 2 is an enlarged view of a portion of Figure 1;

Figure 3 depicts a top view of a stator and rotor of an electric motor drive having a plurality of rotor sensing slots according to another preferred embodiment of the present invention;

Figure 4 is an enlarged view of a portion of Figure 3;

Figure 5 depicts a top view of a stator and rotor of an electric motor drive having a plurality of rotor sensing slots according to another preferred embodiment of the present invention;

Figure 6 is an enlarged view of a portion of Figure 5;

Figure 7 depicts a top view of a stator and rotor of an electric motor drive having a plurality of rotor sensing slots according to another preferred embodiment of the present invention; and

5 Figure 8 is an enlarged view of a portion of Figure 7.

Description of the Preferred Embodiment(s)

Referring now to Figures 1 and 2, an electric machine drive 9 having a complete rotor 10 and stator 12 is depicted. The rotor 10 has a plurality of rotor bars 14 uniformly spaced around the rotor 10. Further, the rotor 10 has a plurality of rotor sensing slots 16 uniformly spaced along its outer periphery 18. The sensing slots 16 have a uniform depth and width. The stator 12 has a plurality of stator slots 20.

The number of sensing slots 16, here twenty-eight, is chosen so that their combination with the stator slots 20, here twenty-four, creates a desired saliency. The use of separate sensing slots 16 results in an effective decoupling between the sensing and torque producing functions. This significantly reduces the potential for ripple torque, cogging torque, or saturation effects.

Another major advantage to using separate sensing slots 16 is that the sensing slots 16 do not have to be skewed if the rotor bars 14 are skewed. Instead, the rotor sensing slots 16 may remain parallel to the stator slots 20 (even if the stator

slots 20 are skewed), resulting in a much larger saliency magnitude.

In another preferred embodiment of the present invention, as depicted in Figures 3 and 4, the spacing between the sensing slots 16 is varied in a repeating manner, sinusoidal for example, to create the desired saliency. For example, a period of variation equal to the pole pitch of the electric machine drive 9 would result in strong coupling between the sensing slots 16 and the fundamental of the machine stator windings (not shown), creating a relatively large saliency ideal for "sensorless control." Such a variation is shown in Figures 3 and 4 as a four-pole induction machine. Since the sensing slots 16 are not used for any function other than to create the desired saliency, the number of sensing slots 16, in Figure 3 and 4 being thirty-five slots 16, can be chosen to optimize the desired saliency.

20 In another preferred embodiment of the present invention, as depicted in Figures 5 and 6, the depth of the sensing slots 16 are varied in a repeating pattern. As an example, a period of variation equal to the pole pitch of the electric drive machine 9 would result in a strong coupling between the sensing slots 16 and the fundamental of the machine stator windings (not shown), creating a large saliency ideal for "sensorless control." Such a variation is depicted Figures 5 and 6 as a four-pole induction machine. As the sensing slots 16 are not used for any function other than to create the

desired saliency, the number of sensing slots 16 can be chosen to optimize the desired saliency.

A fourth preferred method for creating the desired rotor position dependent saliency using separate sensing slots 16 is depicted in Figures 7 and 8. In this preferred embodiment, the width of the uniformly spaced sensing slots 16 is varied in a repeating pattern. As an example, a period of variation equal to the pole pitch of the machine 9 would result in a strong coupling between the sensing slots 16 and the fundamental of the machine stator windings, creating a relatively large saliency ideal for "sensorless control." A four-pole machine is depicted in Figures 7 and 8. Again, as above, because the sensing slots 16 have no function other than to create the desired saliency, the number of sensing slots 16 can be chosen to optimize the desired saliency.

The advantages to creating a rotor position dependent saliency using separate sensing slots 16 are numerous and significant. First, since the sensing slots 16 are not used for any function other than to create the desired rotor position dependent saliency, the number of sensing slots 16 can be chosen independently of the number of rotor bars 14 and becomes an important design variable. This is in direct contrast to the prior art, wherein the number of rotor bars significantly limits the potential for creating saliency.

Second, as the sensing slots 16 are not tied to the rotor bars 14 in any way, skewing of the

rotor bars 14 does not reduce the saliency magnitude significantly. Instead, the sensing slots 16 can be designed to remain parallel to the stator slots 20, even if the stator slots 20 are skewed, thereby
5 maximizing potential for creating a desired saliency.

Third, the effects of saturation on the saliency is minimized since the fundamental flux near the sensing slots 16 will typically be parallel to the sensing slots 16. This is in contrast to methods
10 listed in the prior art that created a saliency by varying the rotor bar slot openings in some manner. It is well known that leakage flux due to the fundamental excitation causes saturation in these structures at relatively low levels of excitation.

Fourth, the use of sensing slots 16 separates the sensing function from the torque producing mechanism of the machine 9. This significantly increases the ability to create saliency without significantly affecting the
15 fundamental operation of the machine 9, resulting in lower torque ripple and cogging torque.

Finally, the creation of sensing slots can be used equally well in pre-existing or new machine designs. The methods listed in the prior art exhibit
20 significant limitations when applied to pre-existing machines in an attempt to retrofit them for "sensorless control."

A related potential advantage to the use of separate sensing slots 16 is the possibility for
30 simplified manufacturing when compared to most prior

art methods. These methods require keeping track of the orientation of laminations during the assembly process in order to create the desired saliency. The sensing slots 16 of the present invention, on the
5 other hand, can be created during a post-assembly step, thereby significantly reducing the complexity of the assembly process.

While the invention has been described in terms of preferred embodiments, it will be
10 understood, of course, that the invention is not limited thereto since modifications may be made by those skilled in the art, particularly in light of the foregoing teachings. For example, the plurality of sensing slots 16 could be introduced to create
15 rotor position dependent saliency in induction machines, Lundell-type synchronous machines, buried permanent magnet synchronous machines, and surface permanent magnet synchronous machines.